

## Lecture 2 – Control Reversal of the typical section

Consider now the typical aerofoil section with a \_\_\_\_\_ attached at the \_\_\_\_\_ as shown in the figure.

*Figure 1 – Typical aerofoil with a control surface*

The section is allowed to \_\_\_\_\_ as indicated by the rotation spring located at the \_\_\_\_\_. There is another degree-of-freedom, which is the \_\_\_\_\_ indicated by \_\_\_\_\_, defined as \_\_\_\_\_ (trailing edge down).

Deflecting the aileron in the positive  $\beta$  direction will cause a change in the pressure distribution pattern over the section, hence resulting in

1. \_\_\_\_\_ and
2. \_\_\_\_\_

Both aerodynamic loadings are evaluated at the \_\_\_\_\_.

The effects of these changes are

1. the extra lift works towards \_\_\_\_\_ motion of the aerofoil
2. the negative pitching moment works towards \_\_\_\_\_ motion of the aerofoil

From this analysis, it can be seen that there will come a point where with an increase in airspeed will result in both of these forces cancel each other out and the aileron becomes ineffective, i.e. aileron deflection  $\beta$  does not produce extra lift.

## Analysis of Aerodynamic Forces

Let us consider the rotational equilibrium of the aerofoil in figure 1.

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[EQN.1]

where  $e$  is the distance between the elastic axis and the aerodynamic centre. Recalling that the lift and pitching moment of a two-dimensional aerofoil are given by

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When the aileron is deflected by  $\beta$ , the effective camber will produce a change in lift and moment. Assuming that the angles  $\alpha$  and  $\beta$  are small so they are in the linear region, we obtain

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[EQN.2]

where

$C_{L\alpha}$	Lift curve slope of the aerofoil, i.e. $\frac{dC_L}{d\alpha}$
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$C_{L\beta}$	Lift curve slope of the aileron, i.e. $dC_L/d\beta$
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$C_{M\beta}$  Moment curve slope of the aileron, i.e.  $dC_M/d\beta$ . Note that  $C_{M\beta} < 0$

$C_{M0}$  Zero lift pitching moment.  $C_{M0} = 0$  for a symmetric aerofoil

Now, let us substitute the aerodynamic terms into the equilibrium equation in rotation (equation 1) to give

Recall that  $\alpha = \alpha_r + \theta$ . We can rewrite the above expression as

\_\_\_\_\_  
 Note the existence of divergence. Substitute the expression for  $\theta$  into equation 2a to obtain

\_\_\_\_\_  
 Let us now consider the \_\_\_\_\_ in the above expression, especially the term in the brackets involving  $\beta$ .

- The first term  $C_{L\beta}\beta$  is \_\_\_\_\_.

It directly gives an increase in lift with a change in angle  $\beta$ .

- The term  $C_{L\beta} \frac{cqSC_{L\alpha}C_{M\beta}}{kC_{L\beta}}\beta$  is more complex but it clearly represents the \_\_\_\_\_  
 \_\_\_\_\_. Recall that  $C_{M\beta} < 0$ ,  
 therefore for a positive change in aileron angle  $\beta$ , this term is \_\_\_\_\_  
 and causes a decrease in lift.

At low speed (small value of  $q$ ), the increase in  $\beta$  will result in higher lift, so the aircraft control works as intended. However as the flow speed increases, and so does the dynamic pressure  $q$ , there will come a point where the aeroelastic effects dominate, hence the rate of change of lift with respect to  $\beta$  vanishes, i.e.

\_\_\_\_\_  
 [EQN.3]

We can determine the dynamic pressure where control reversal begins by equating the terms in the brackets in the numerator to be zero, to obtain

\_\_\_\_\_  
 \_\_\_\_\_

The term  $q_R$  is always positive because  $C_{M\beta} < 0$ ,  $C_{L\beta} > 0$  and  $C_{L\alpha} > 0$ . Finally, the reversal speed is given by

\_\_\_\_\_

The parameters affecting the reversal speed are shown in the expression above. The most direct method to increase the reversal speed is to increase the \_\_\_\_\_ of the wing but that will inevitably incur a structural weight penalty. Therefore, a common solution is to position the aileron \_\_\_\_\_ to benefit from the higher torsional stiffness than the section near the wing tip.

### Aileron Effectiveness

The aileron effectiveness can be measured by

$$\eta = \frac{\text{actual change in lift per unit change in } \beta}{\text{change in lift per unit change in } \beta \text{ for a rigid wing}} = \frac{\left( \frac{dC_L}{d\beta} \right)_{\text{with aileron}}}{\left( \frac{dC_L}{d\beta} \right)_{\text{rigid wing}}} = \frac{\left( \frac{dC_L}{d\beta} \right)_{\text{with aileron}}}{C_{L\beta}}$$

Taking the  $\left( \frac{dC_L}{d\beta} \right)$  expression from [EQN.3], we obtain

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For a perfectly rigid wing, both  $q_R$  and  $q_D$  are infinite, so the effectiveness \_\_\_\_\_.